

CUM. DIST. CURVE HLREAR

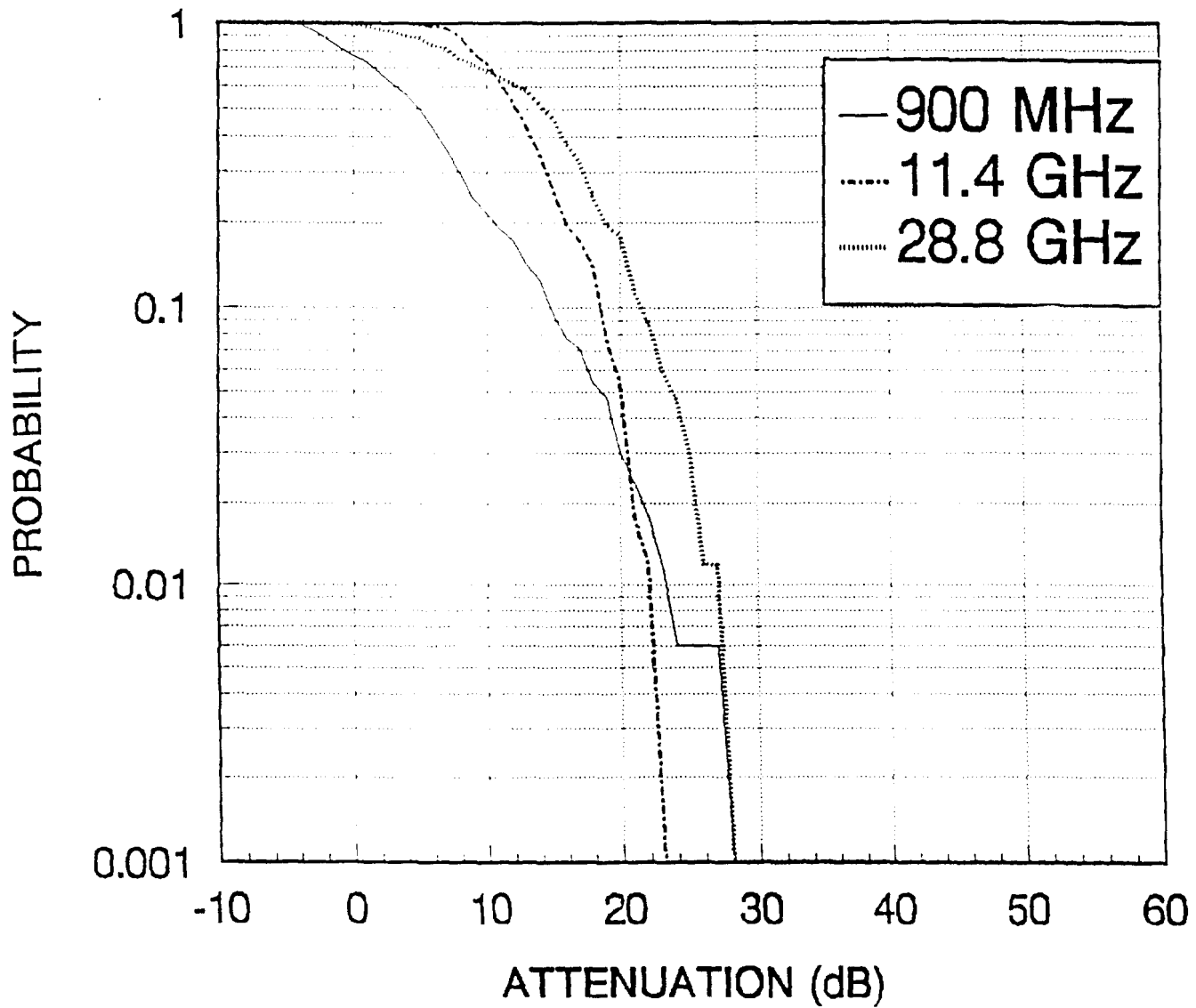


Figure 22. Cumulative distribution for all data in the private residence with two walls between the transmitter and receiver.

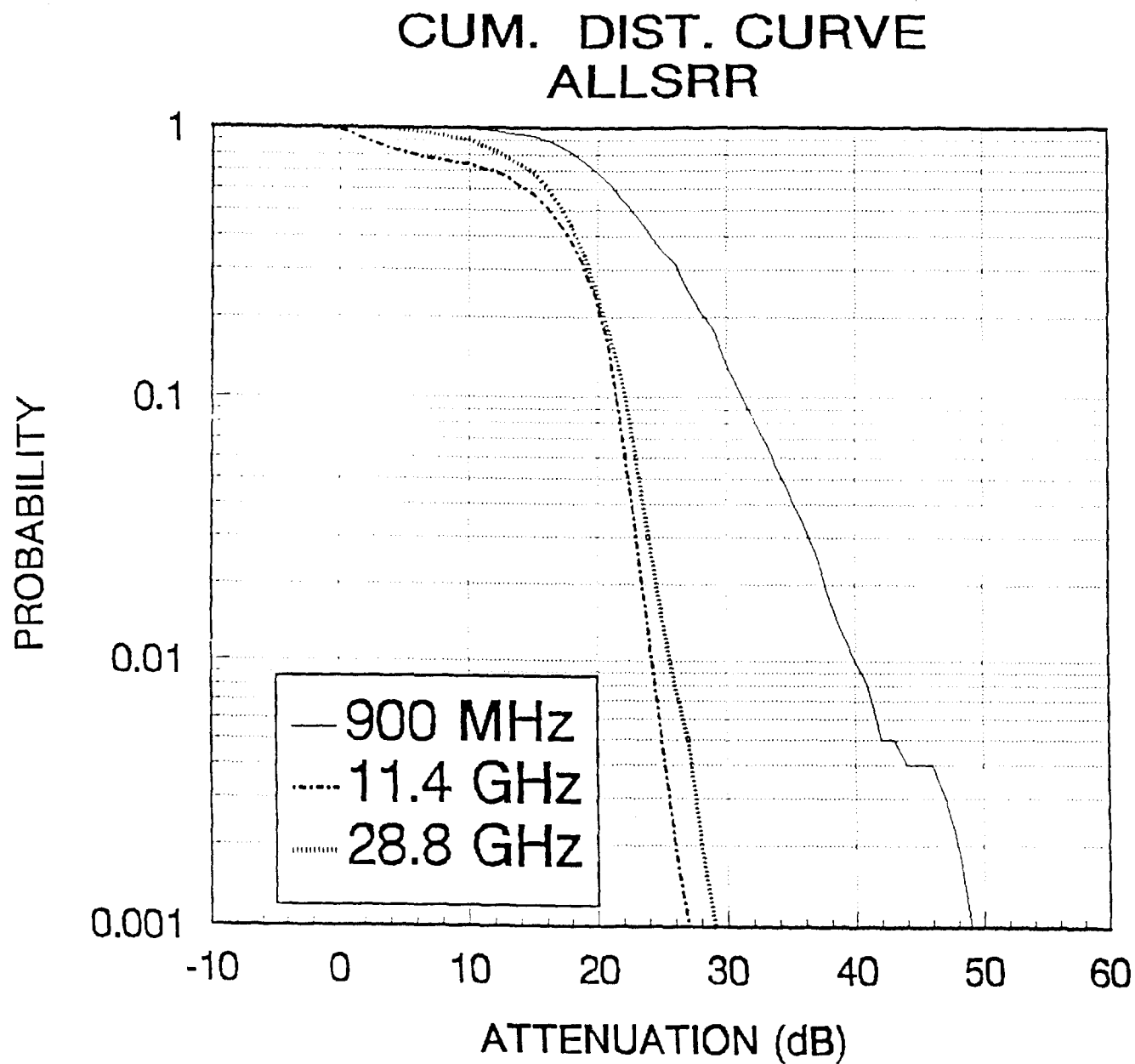


Figure 23. Cumulative distribution for all data in the storeroom building with metal siding.

The maximum attenuation that will be present less than a certain percentage of time can be read off these figures. This number can be used for the link margin at different link reliabilities. Table 4 has the mean attenuation and its standard deviation for all three data combinations. The means at all frequencies are greater for the two-wall case.

Figure 23 shows the cumulative distribution function for all of the data collected in the storeroom (metal structure with metal siding). The mean attenuation and its standard deviation are listed in Table 4. The attenuation is highest (greater than 49 dB less than 0.1 % of the time) at 900 MHz, because of the shielding effect of the metal siding on the building and the small windows (with respect to a wavelength at 900 MHz). The attenuation at 11.4 and 28.8 GHz was greater than 27 and 29 dB respectively less than 0.1 % of the time.

6.0 CONCLUSIONS

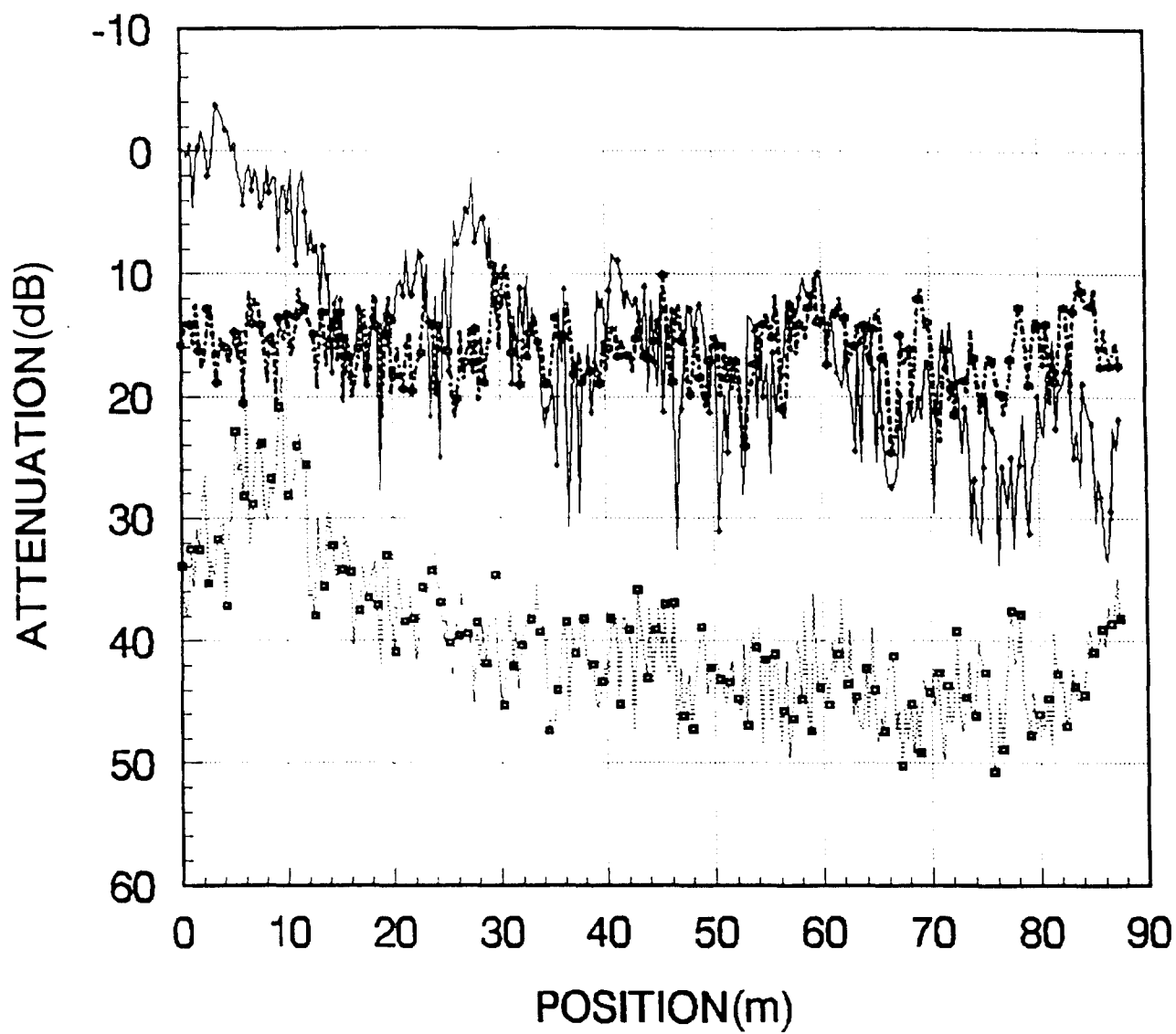
The penetration attenuation for the Radio Building and the private residence tend to increase with frequency. The penetration attenuation for the storeroom decreases with increasing frequency.

The separate cases for the Radio Building and private residence also indicate a progressively increasing amount of penetration attenuation at all frequencies as the number of wall penetrations increase in the building structure.

The electromagnetic energy at 11.4 and 28.8 GHz can couple into the storeroom building more effectively than that energy at 900 MHz. The shielding effectiveness (ratio in dB of the power outside the structure to the power inside the structure) of the structure is less at the two higher frequencies and allows more energy to couple through the walls. The shielding effectiveness of a metal structure is dependent on the size of the openings in the outer shell of the structure. These may be windows, doors, heating and/or air conditioning penetrations, holes, etc. When the size of the opening in the structure is greater than or comparable to a wavelength, then the opening in the structure provides a strong coupling path for electromagnetic energy to flow into or out of the structure. This reduces the penetration attenuation of the structure.

The penetration attenuation values derived from the measurements conducted in this study can be used determine the feasibility of personal communications. The cumulative distribution functions of the penetration attenuation can provide information on what link margins are necessary for different communication probabilities or reliabilities. The penetration attenuation provides a quantitative margin for link calculations to use in analyzing and designing personal communication systems.

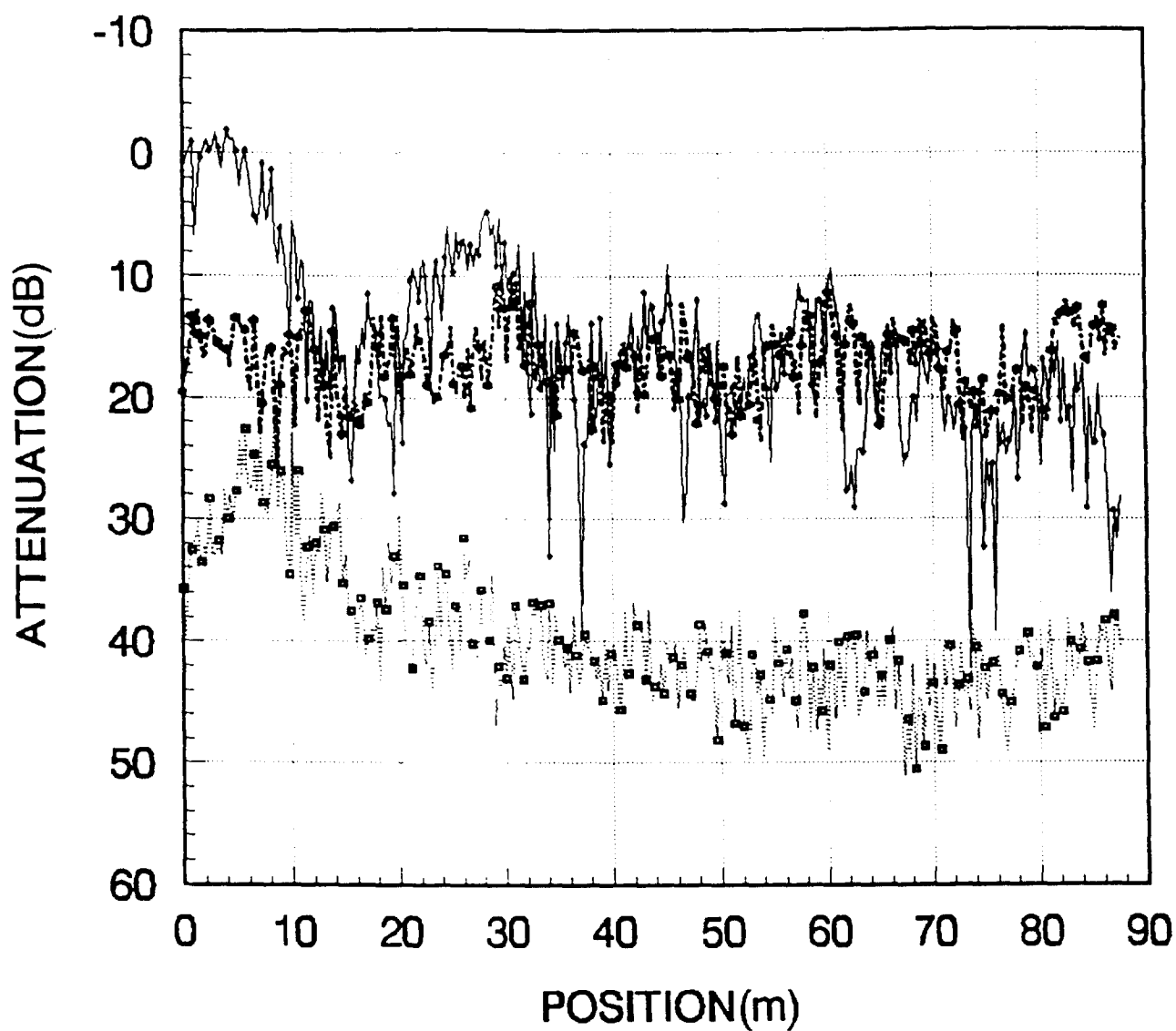
APPENDIX: ATTENUATION PLOTS FOR ALL MEASUREMENT PATHS



RB1D
ATTENUATION

— 900 MHz
--- 11.4 GHz
..... 28.8 GHz

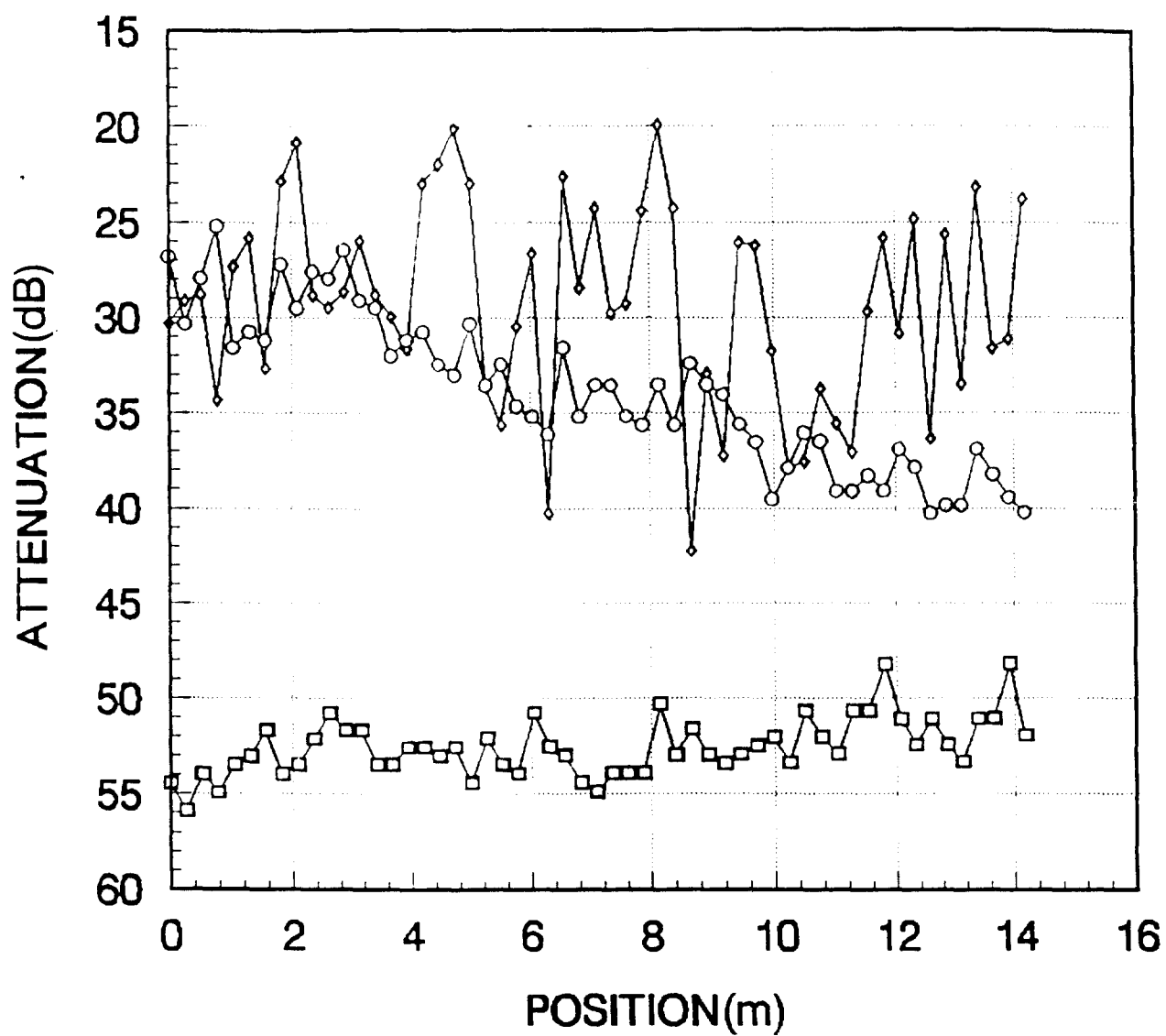
Figure A-1. Penetration loss for Radio Building path RB1D.



RB1E
ATTENUATION

—○— 900 MHz
---○--- 11.4 GHz
...□... 28.8 GHz

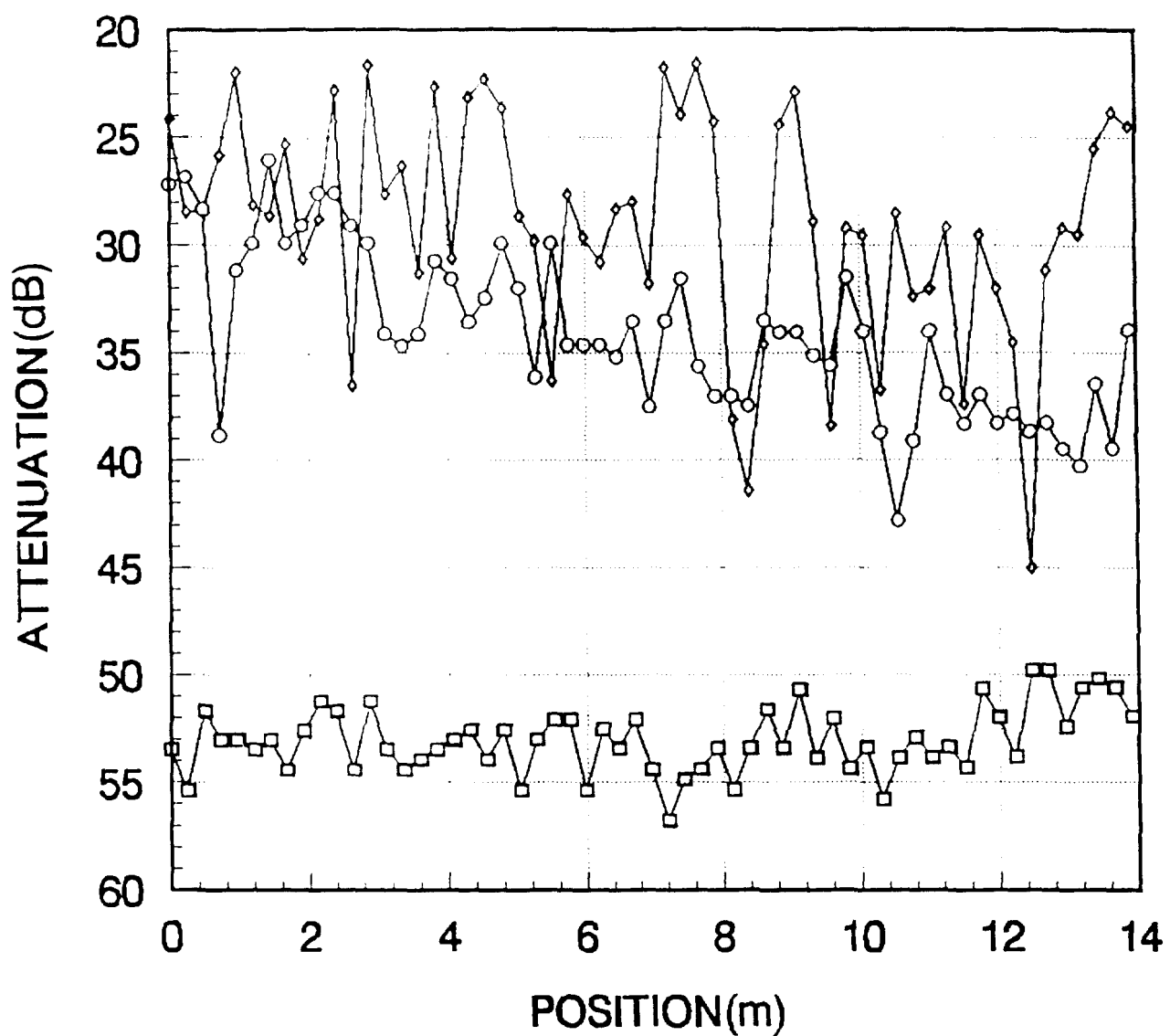
Figure A-2. Penetration loss for Radio Building path RB1E.



RB2B
ATTENUATION

—◇— 900 MHz
—○— 11.4 GHz
—□— 28.8 GHz

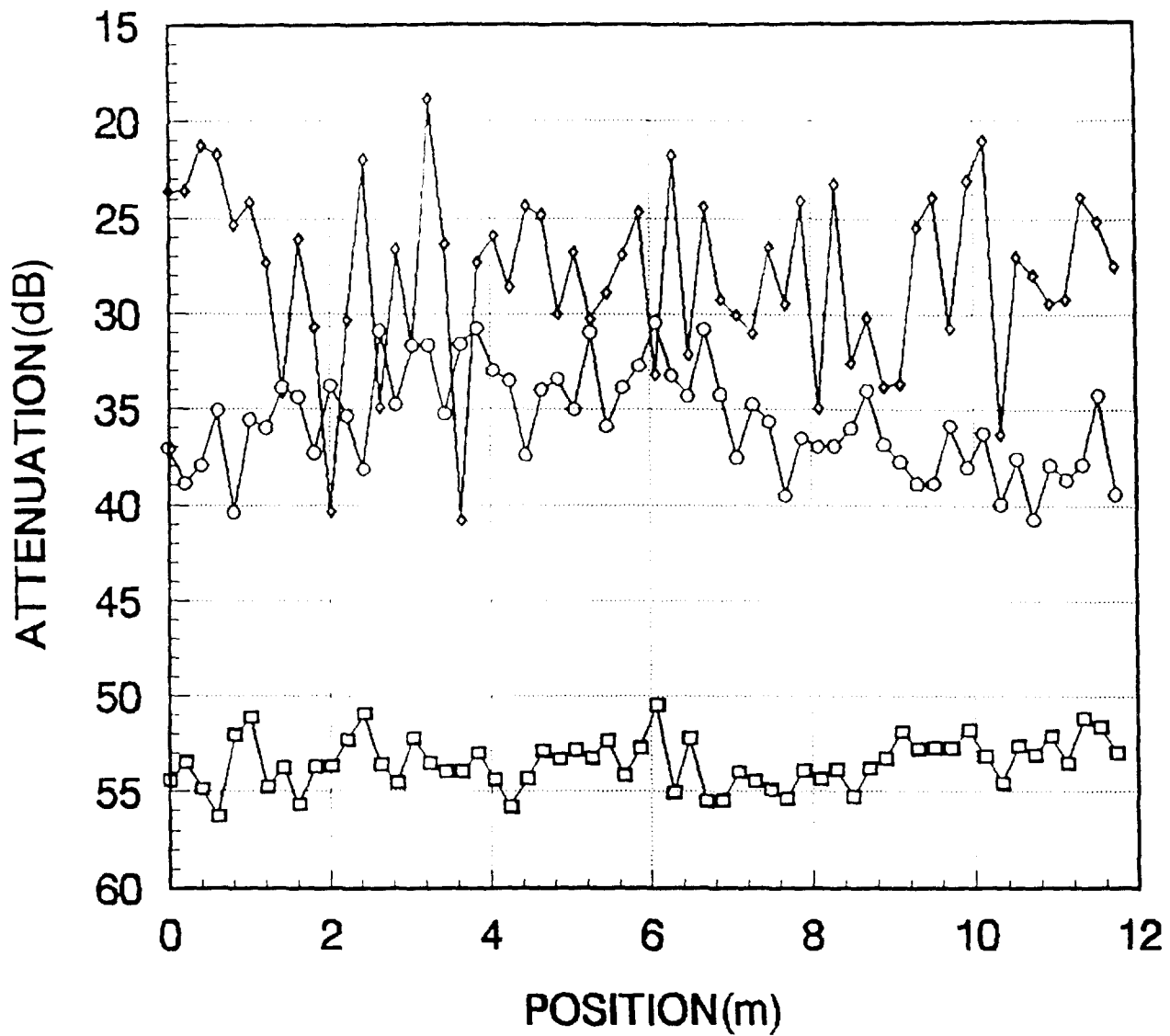
Figure A-3. Penetration loss for Radio Building path RB2B.



RB2C
ATTENUATION

- ◆ 900 MHz
- 11.4 GHz
- 28.8 GHz

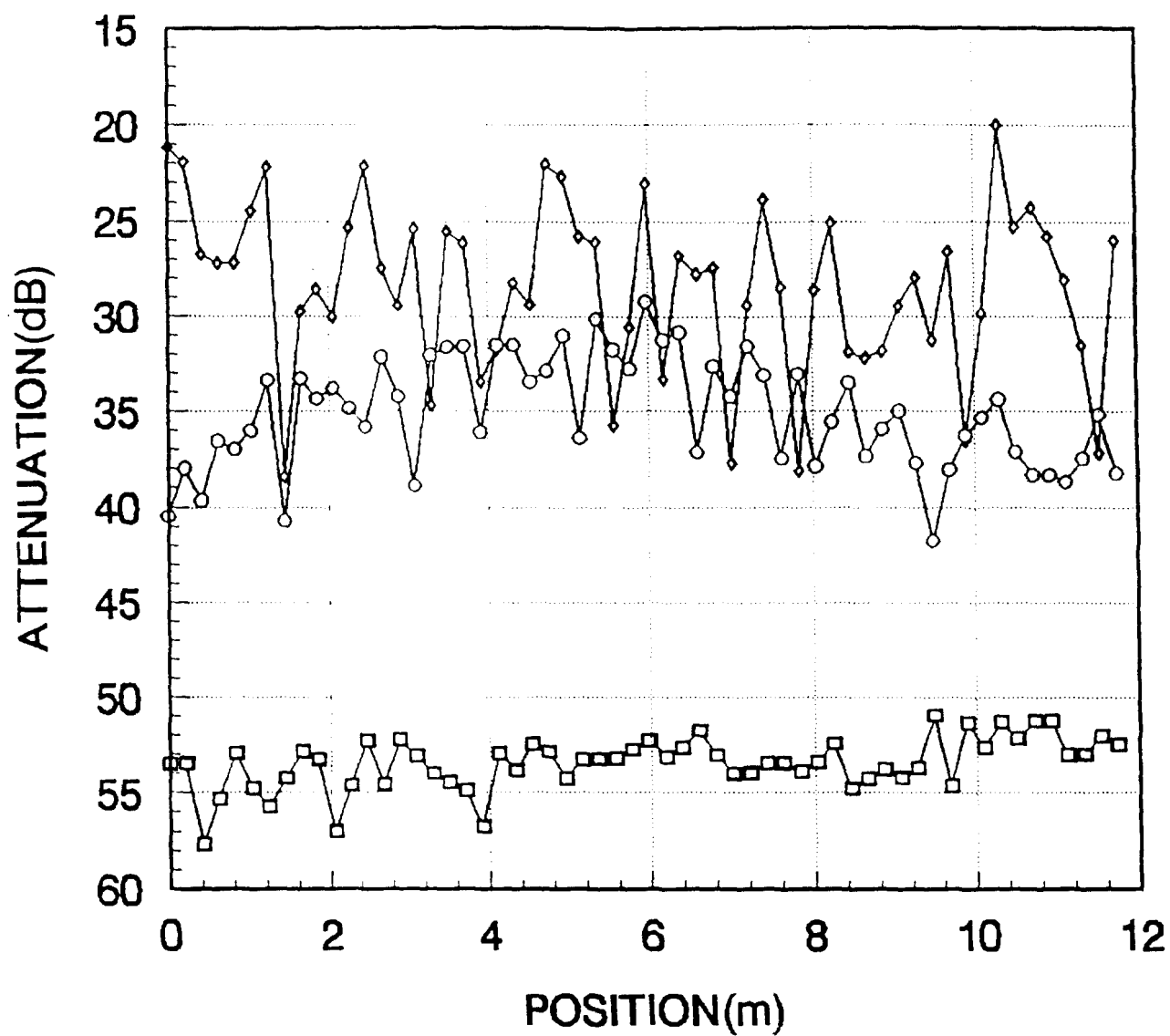
Figure A-4. Penetration loss for Radio Building path RB2C.



RB3B ATTENUATION

◆ 900 MHz
 ○ 11.4 GHz
 □ 28.8 GHz

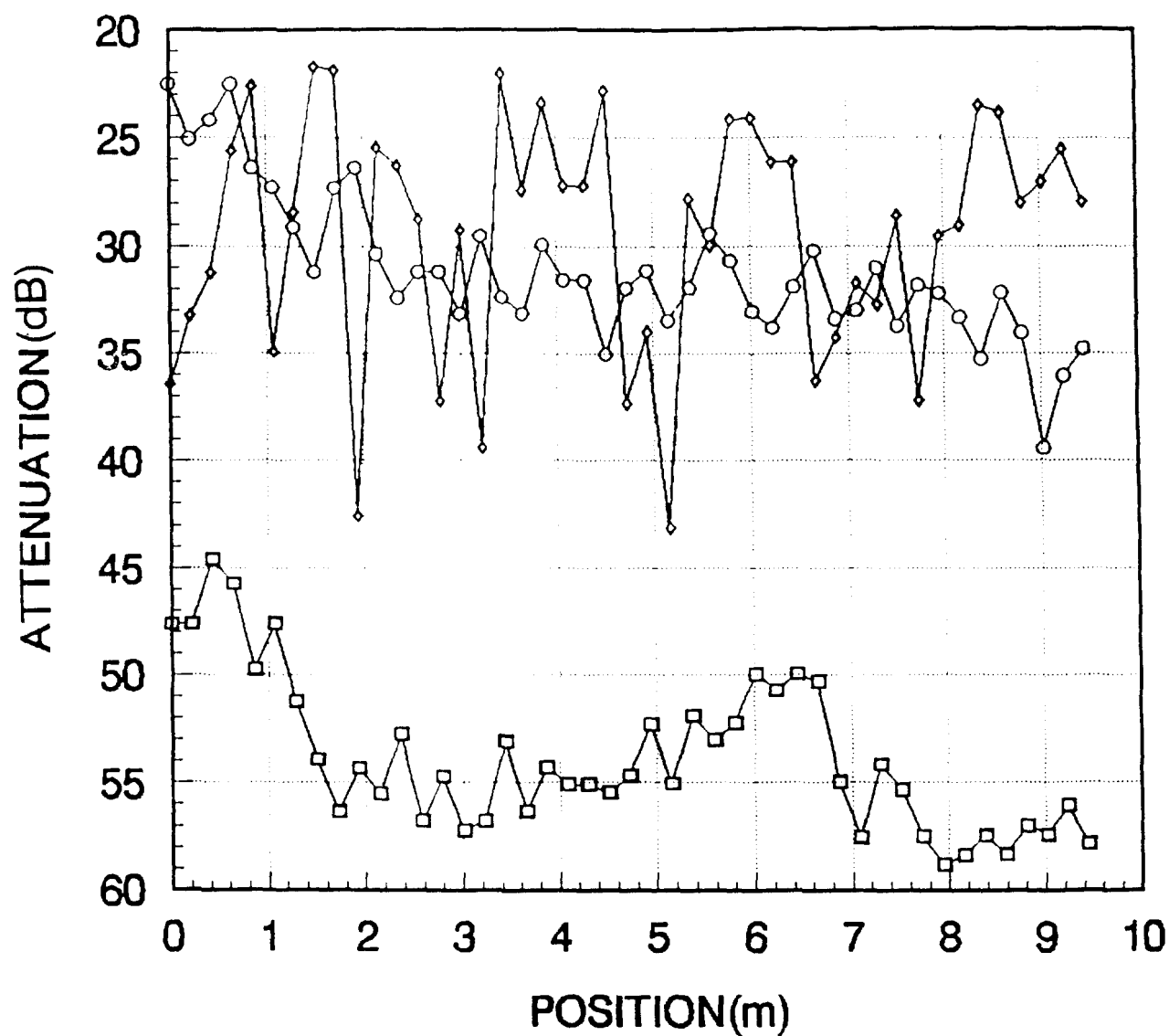
Figure A-5. Penetration loss for Radio Building path RB3B.



**RB3C
ATTENUATION**

—◇— 900 MHz
—○— 11.4 GHz
—□— 28.8 GHz

Figure A-6. Penetration loss for Radio Building path RB3C.



**RB4C
ATTENUATION**

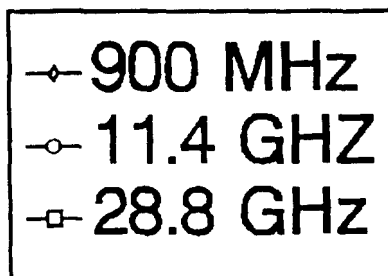
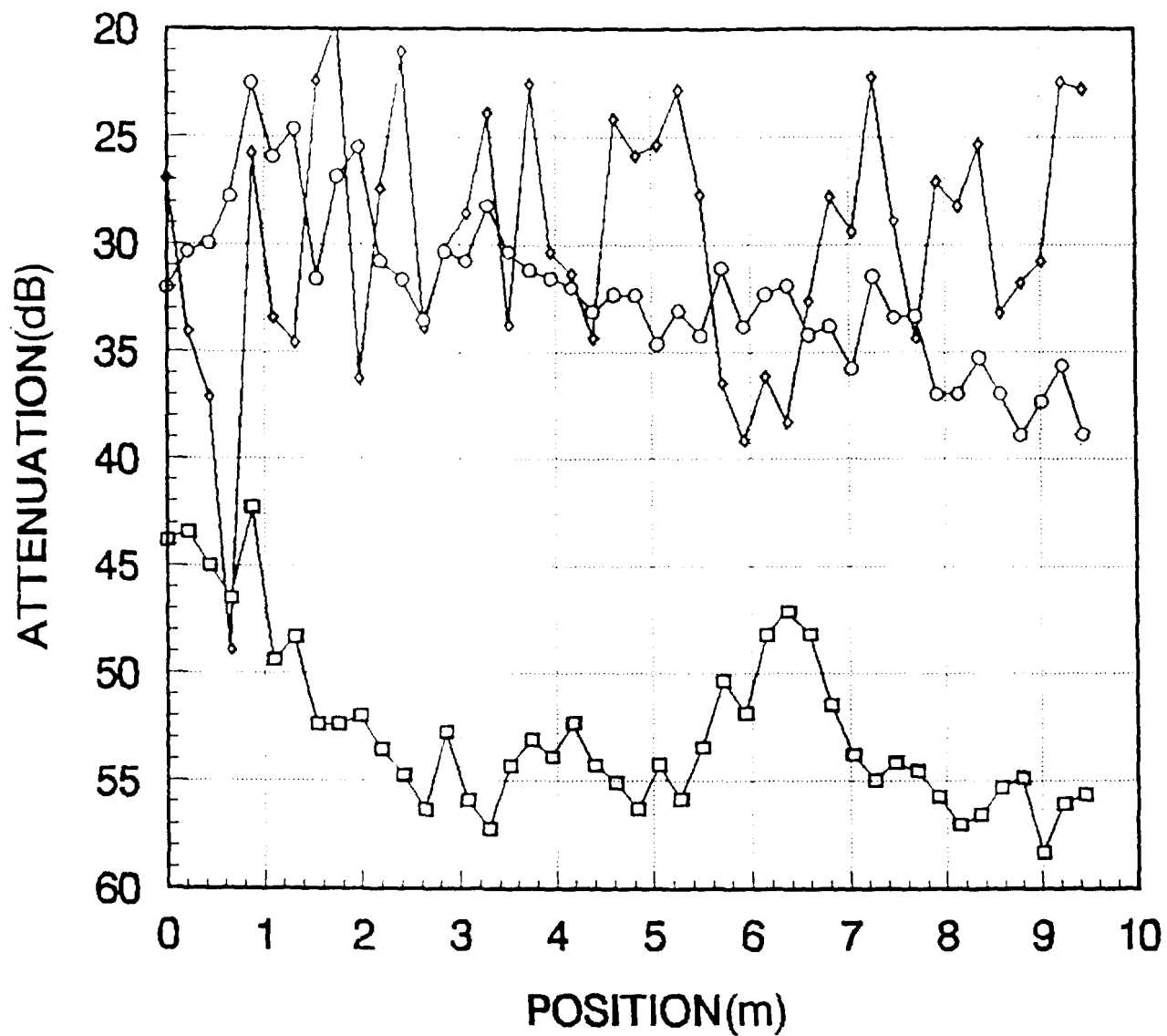


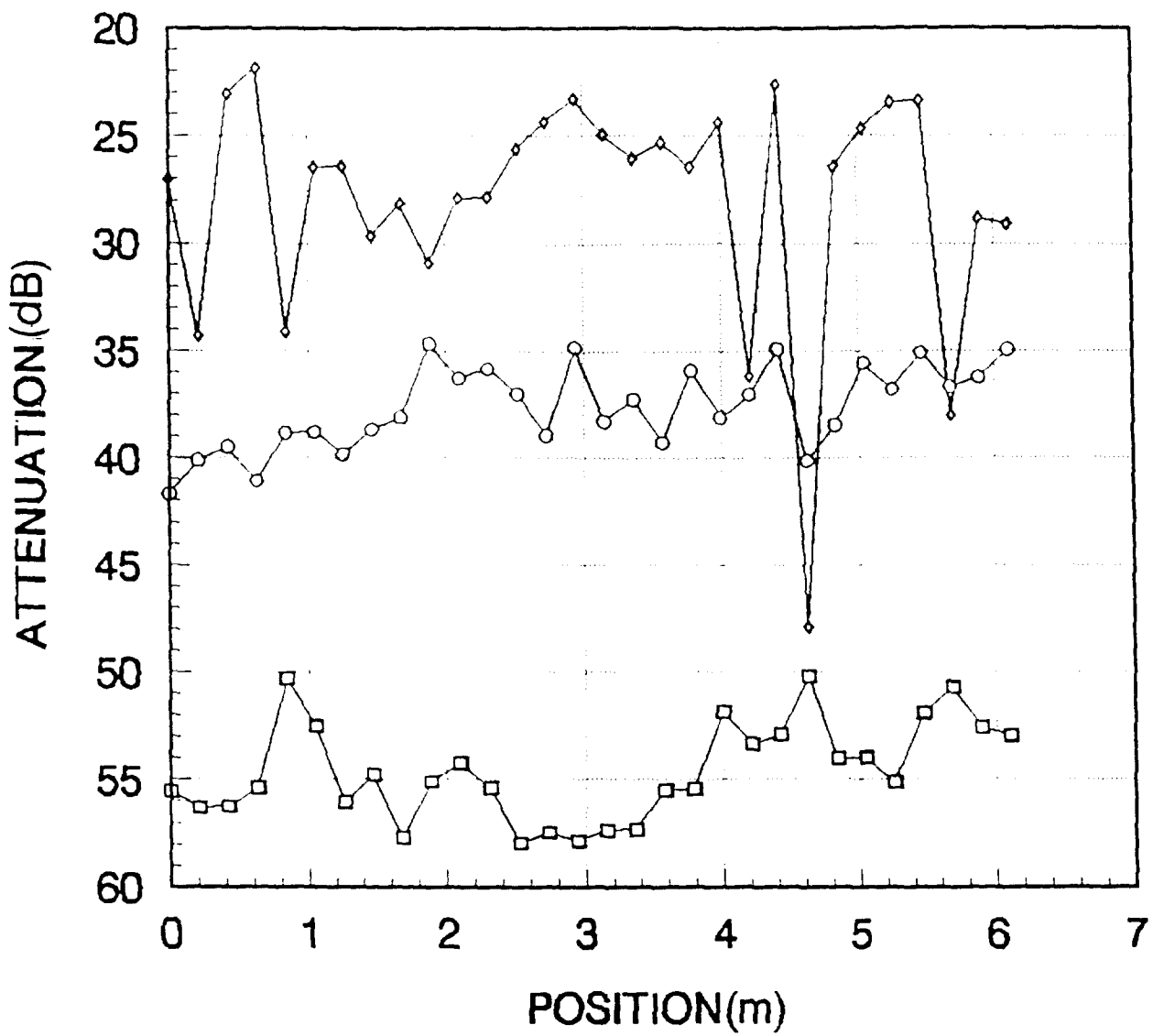
Figure A-7. Penetration loss for Radio Building path RB4C.



RB4D ATTENUATION

—◇— 900 MHz
—○— 11.4 GHz
—□— 28.8 GHz

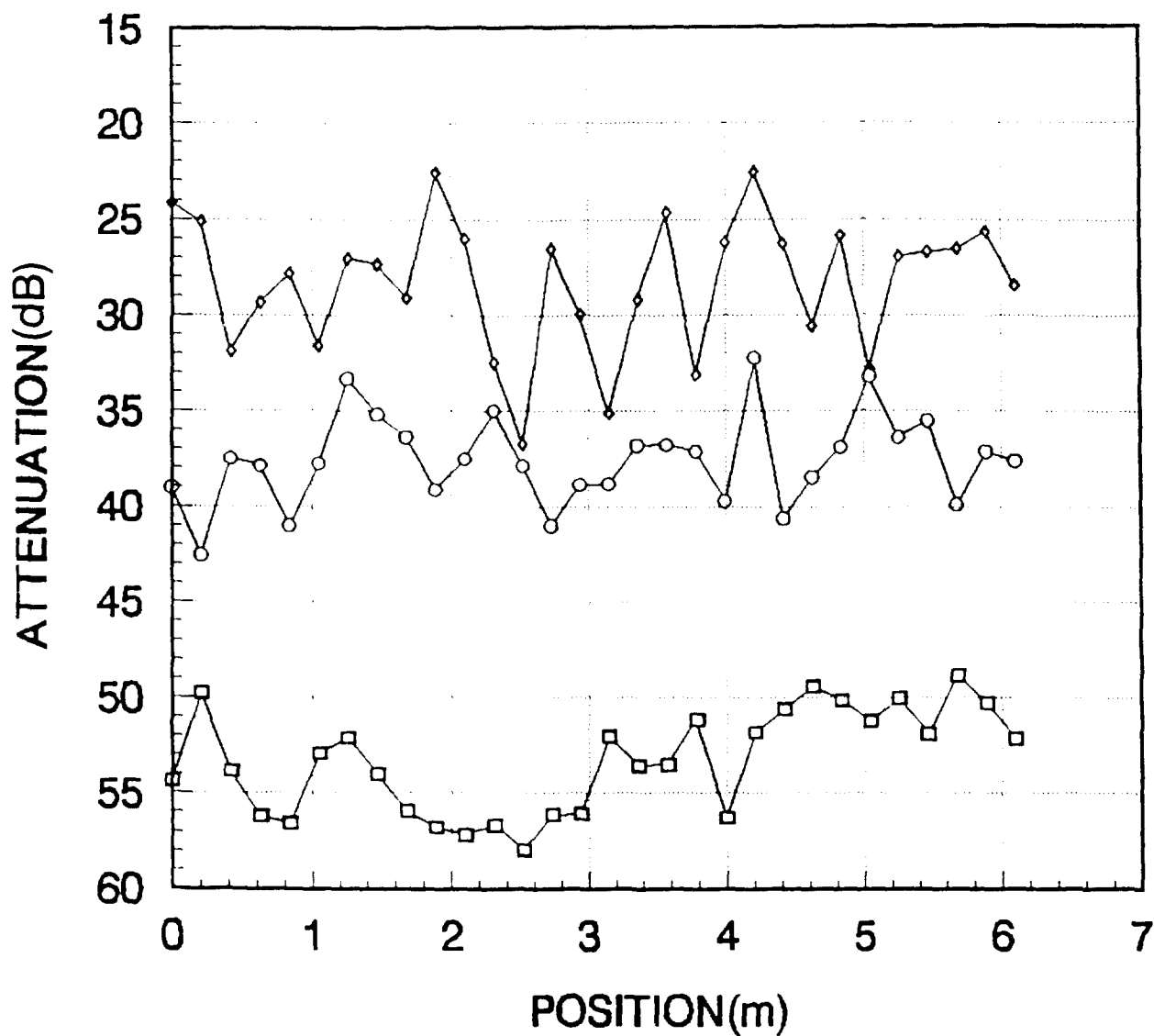
Figure A-8. Penetration loss for Radio Building path RB4D.



**RB5A
ATTENUATION**

—◇— 900 MHz
—○— 11.4 GHz
—□— 28.8 GHz

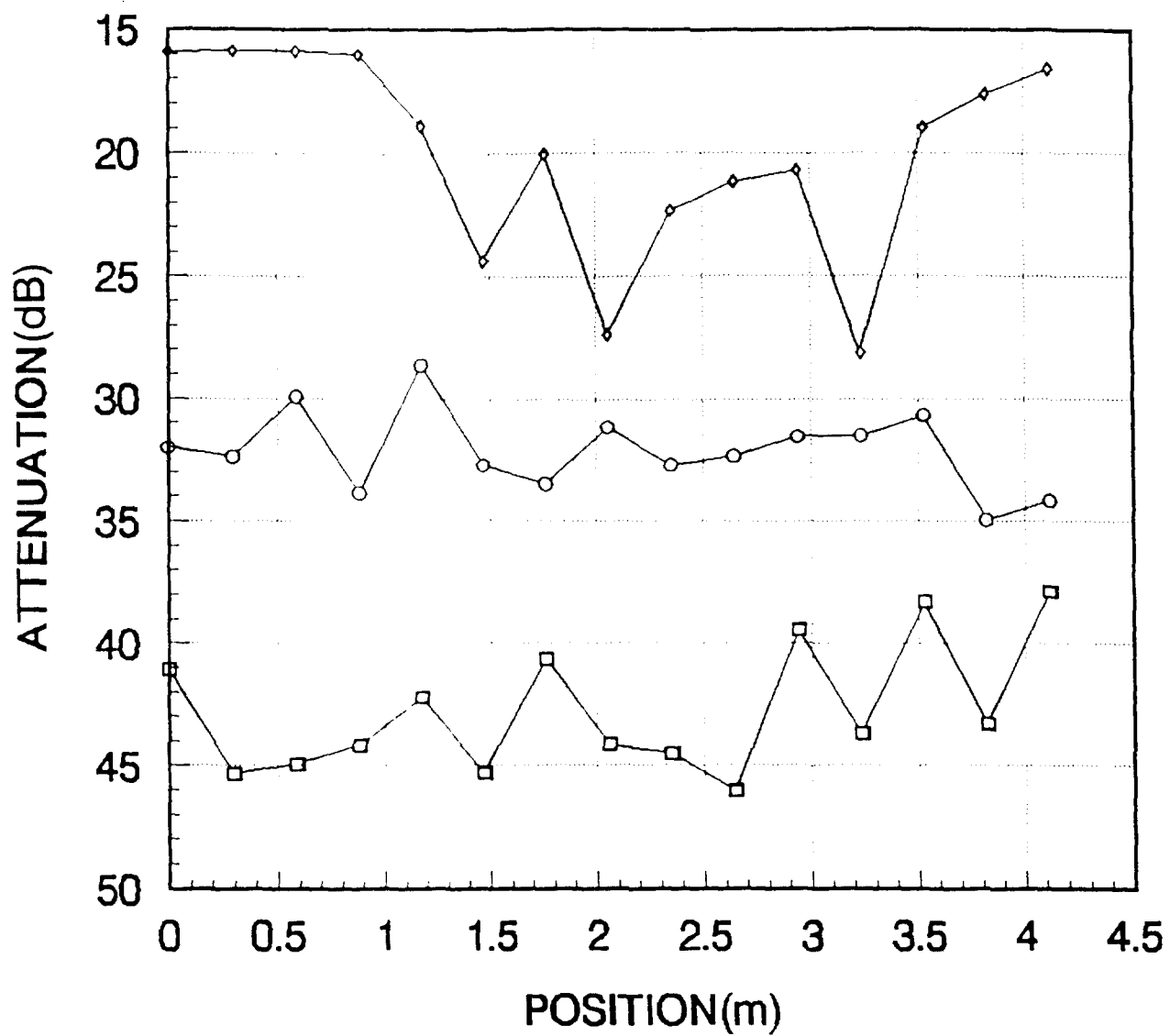
Figure A-9. Penetration loss for Radio Building path RB5A.



RB5B ATTENUATION

◆ 900 MHz
○ 11.4 GHz
□ 28.8 GHz

Figure A-10. Penetration loss for Radio Building path RB5B.



RB6A ATTENUATION

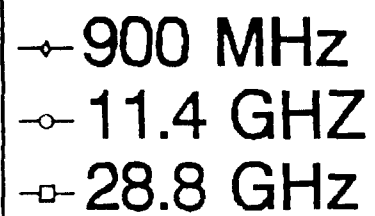
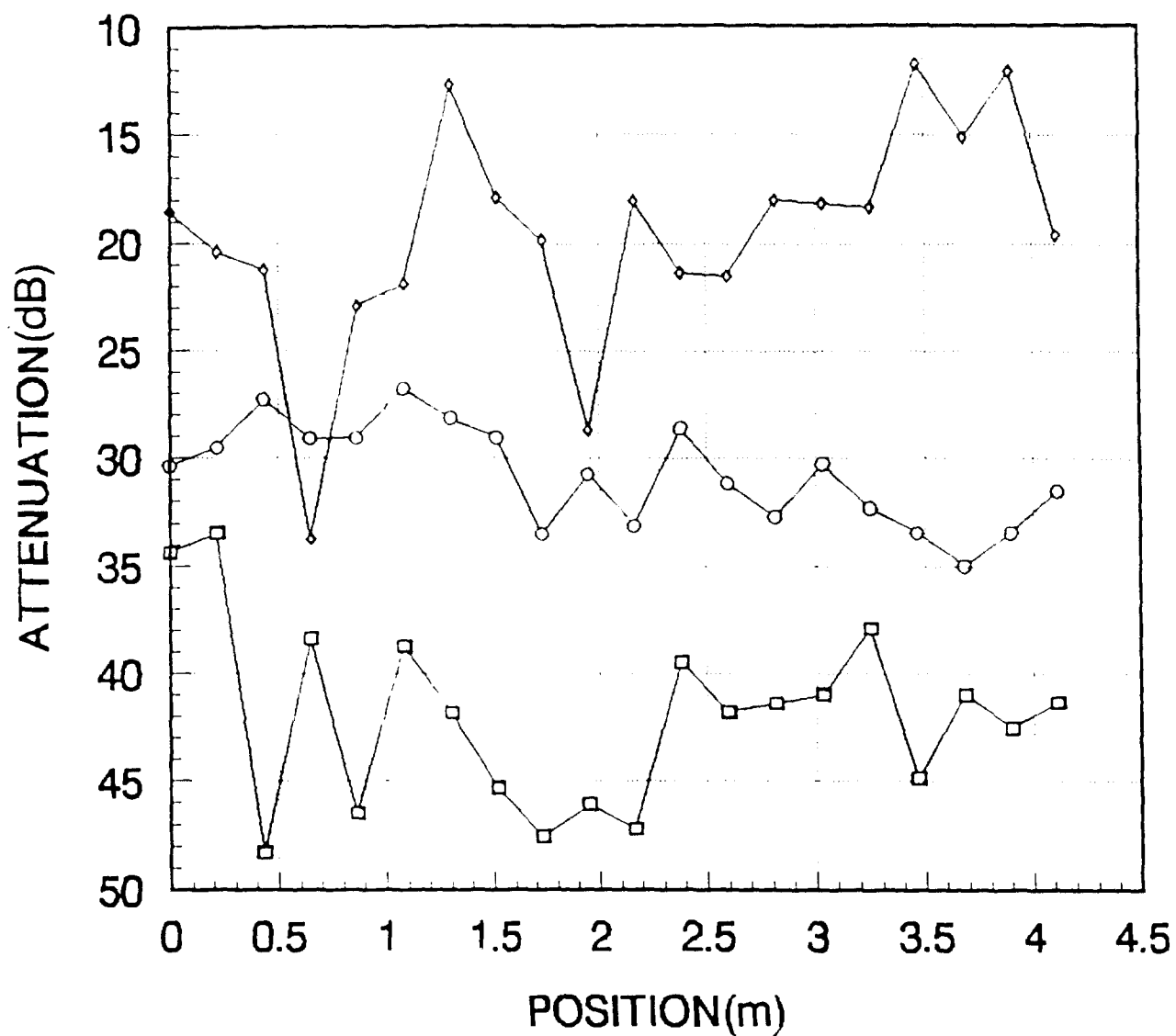


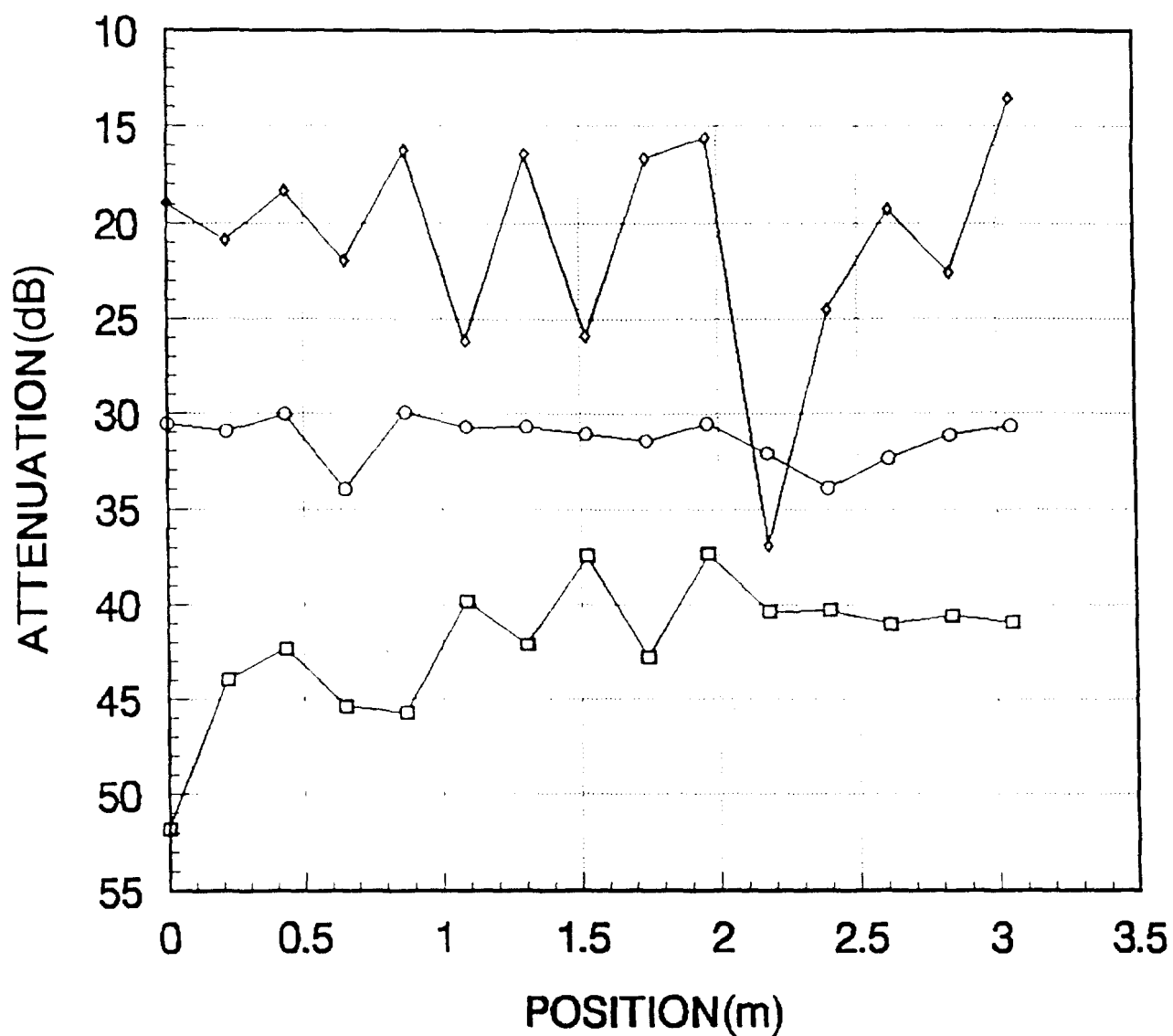
Figure A-11. Penetration loss for Radio Building path RB6A.



RB6B
ATTENUATION

—◇— 900 MHz
—○— 11.4 GHz
—□— 28.8 GHz

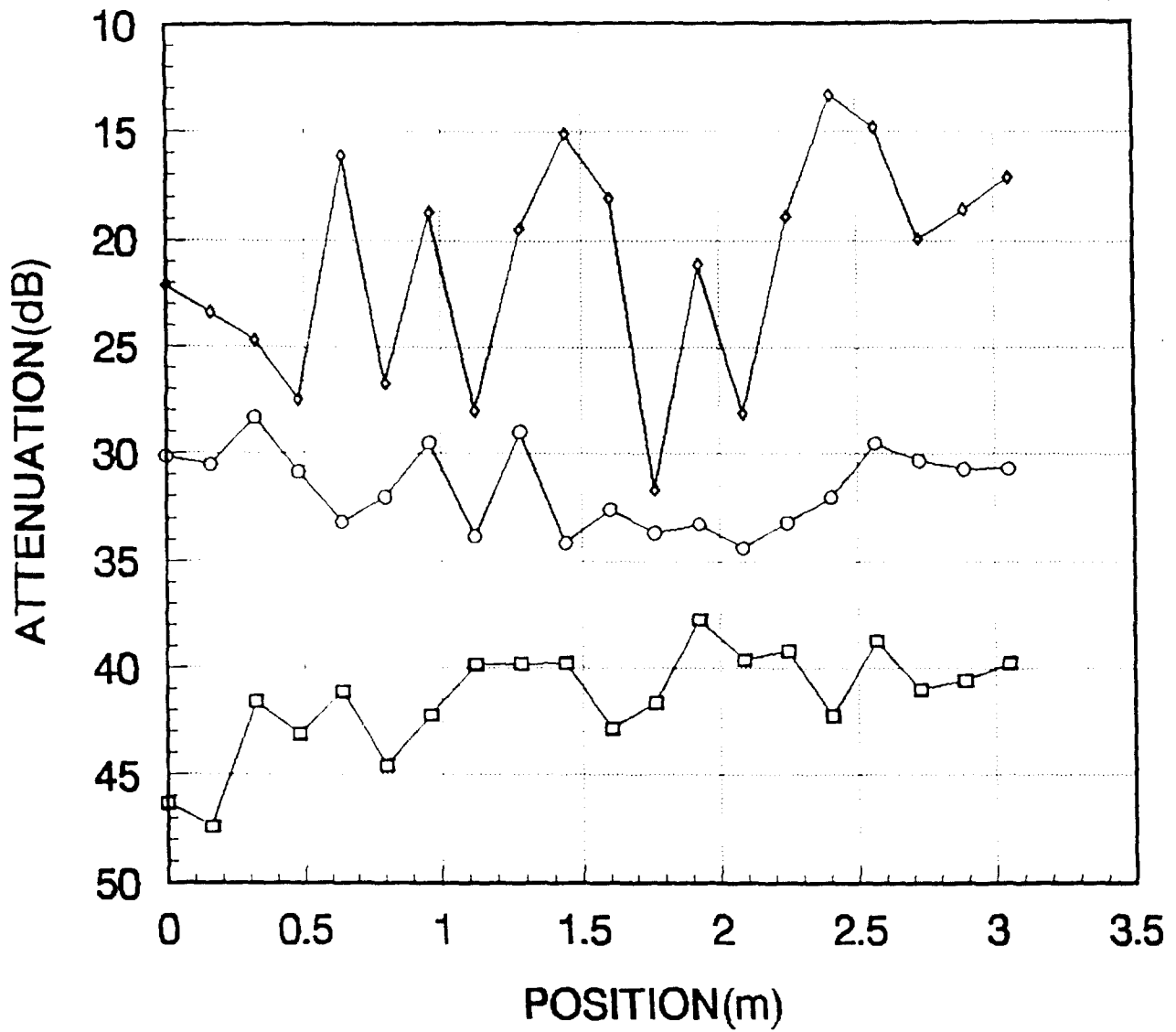
Figure A-12. Penetration loss for Radio Building path RB6B.



**RB7A
ATTENUATION**

◆ 900 MHz
○ 11.4 GHz
□ 28.8 GHz

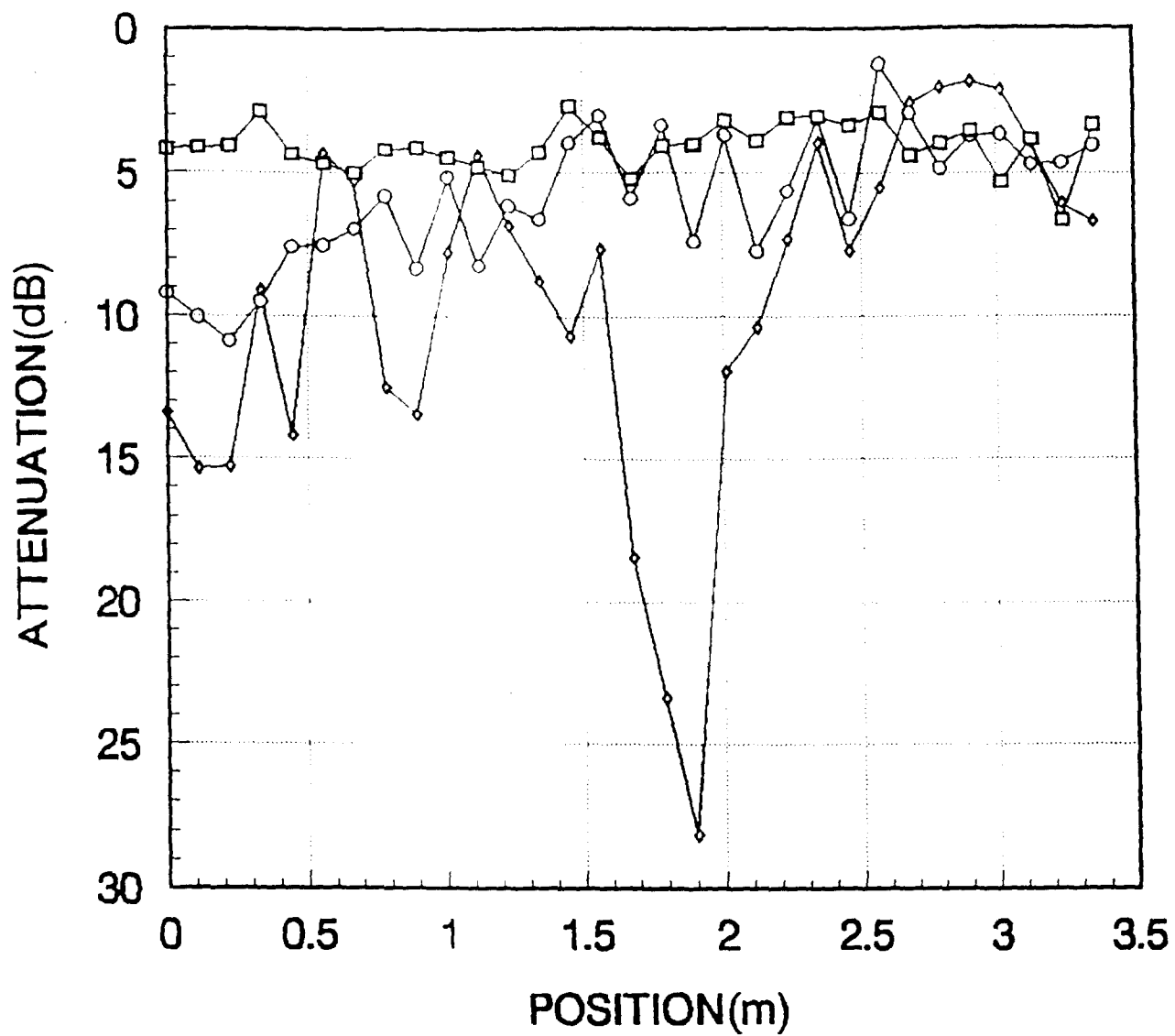
Figure A-13. Penetration loss for Radio Building path RB7A.



**RB7B
ATTENUATION**

- ◆ 900 MHz
- 11.4 GHz
- 28.8 GHz

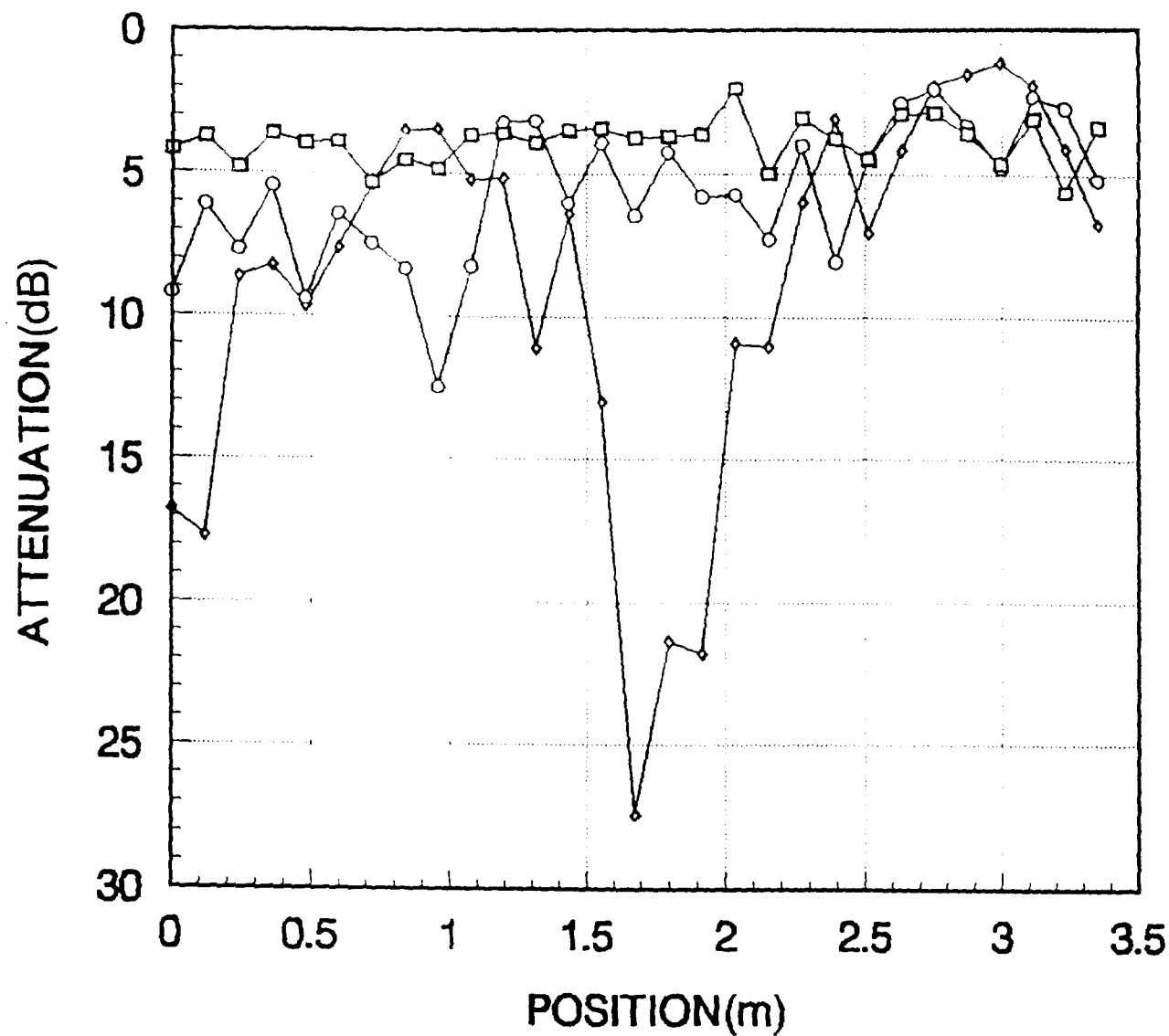
Figure A-14. Penetration loss for Radio Building path RB7B.



RB8A
ATTENUATION

—◇— 900 MHz
—○— 11.4 GHz
—□— 28.8 GHz

Figure A-15. Penetration loss for Radio Building path RB8A.



**RB8B
ATTENUATION**

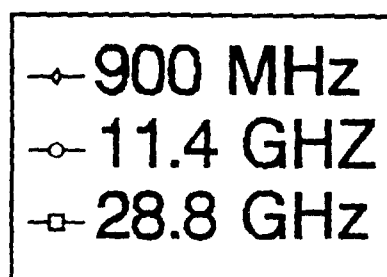
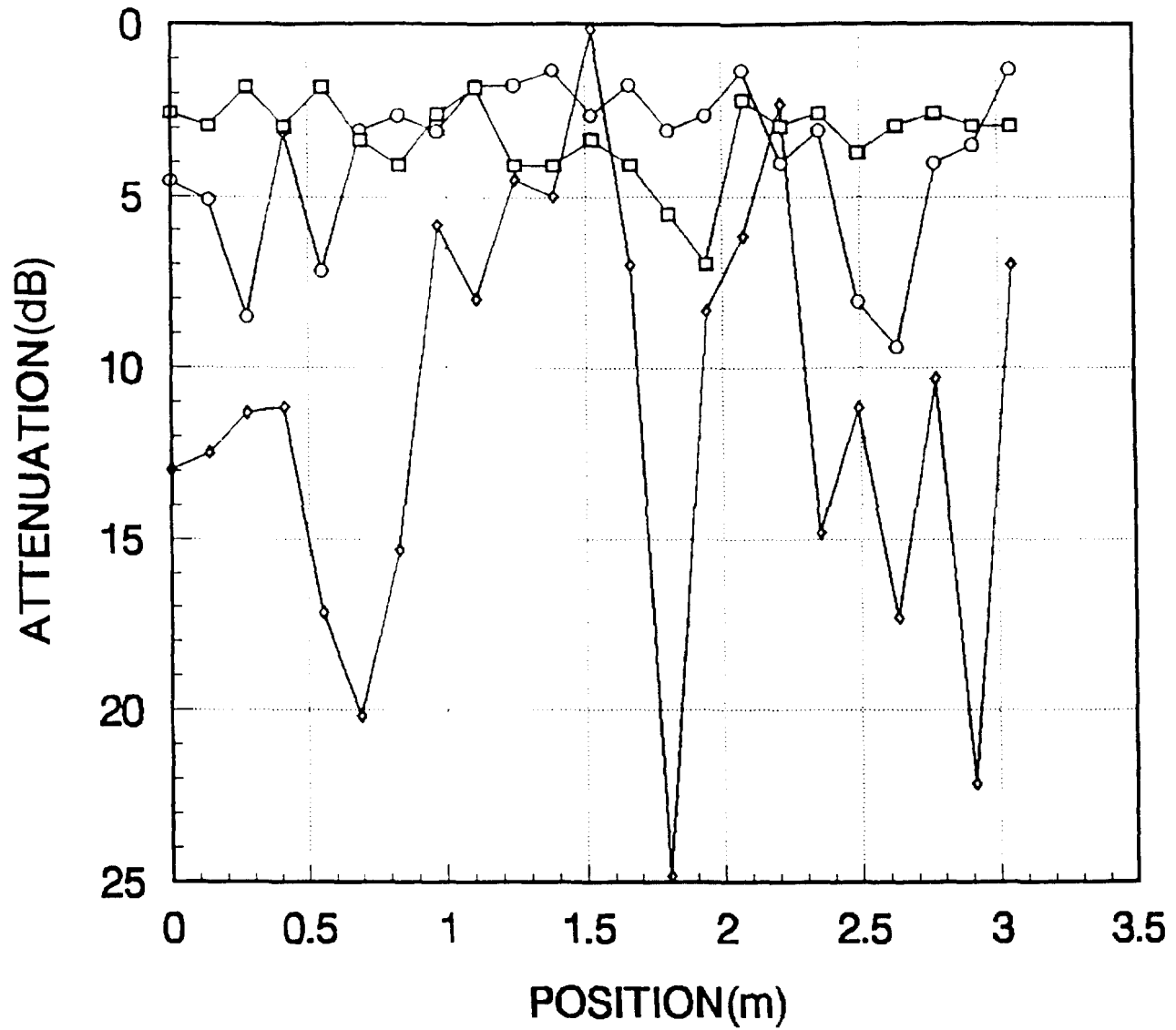


Figure A-16 Penetration loss for Radio Building path RB8B.



RB9A ATTENUATION

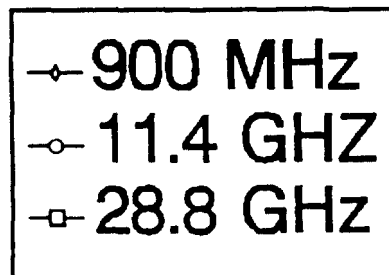
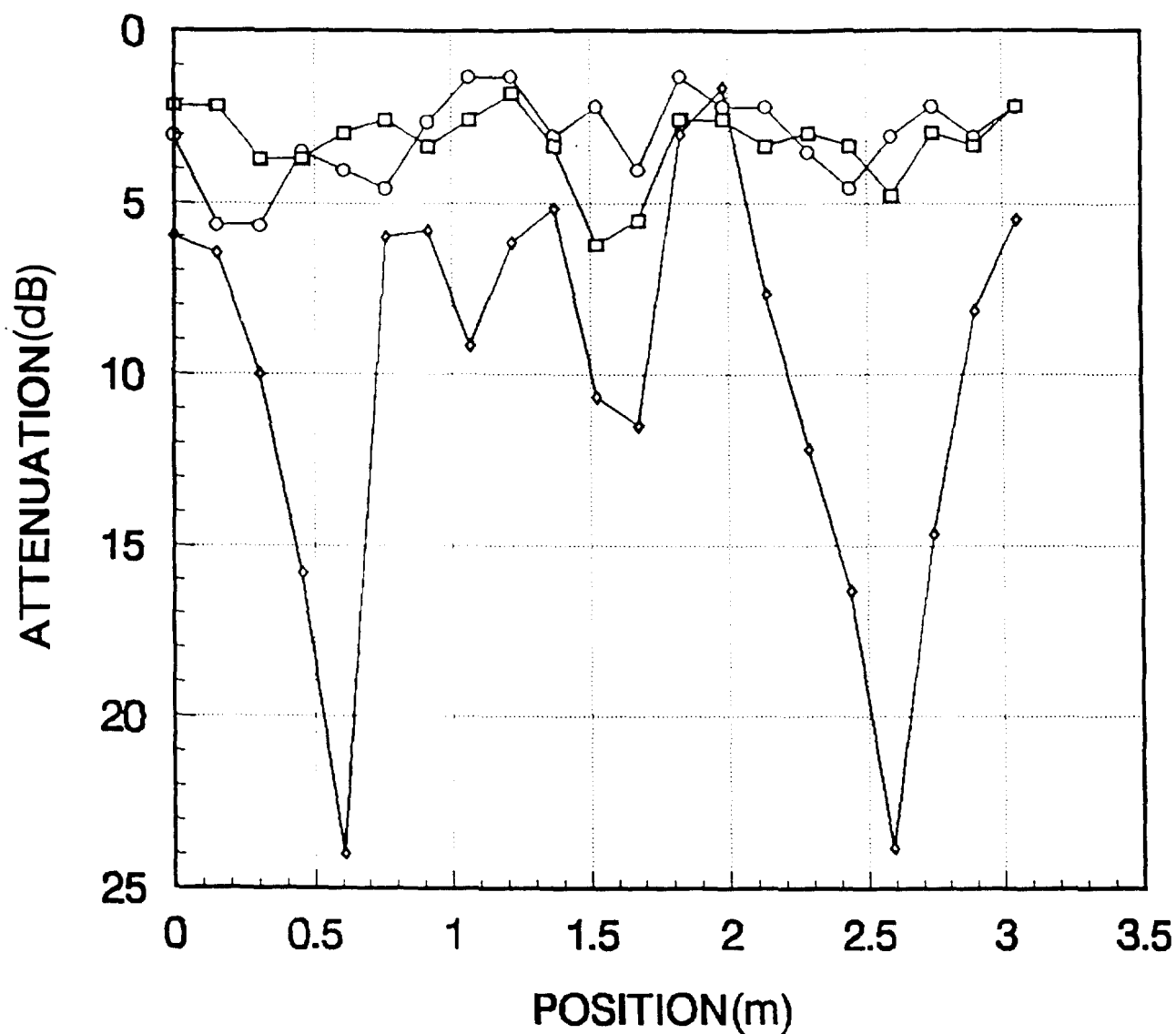


Figure A-17. Penetration loss for Radio Building path RB9A.



RB9B ATTENUATION

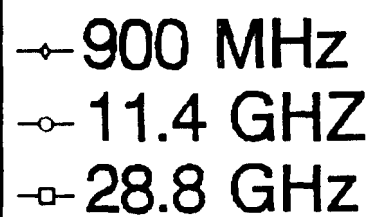
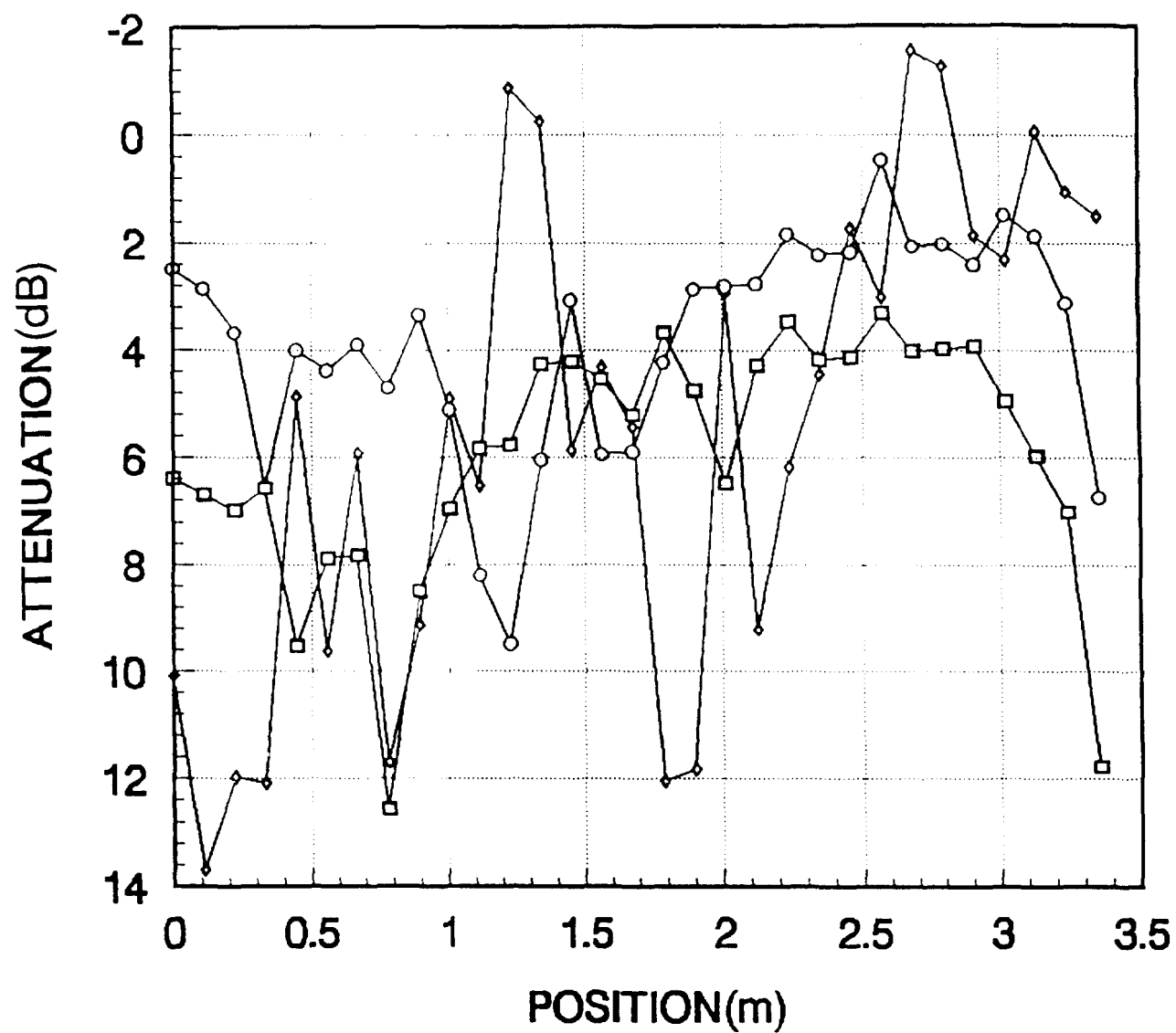


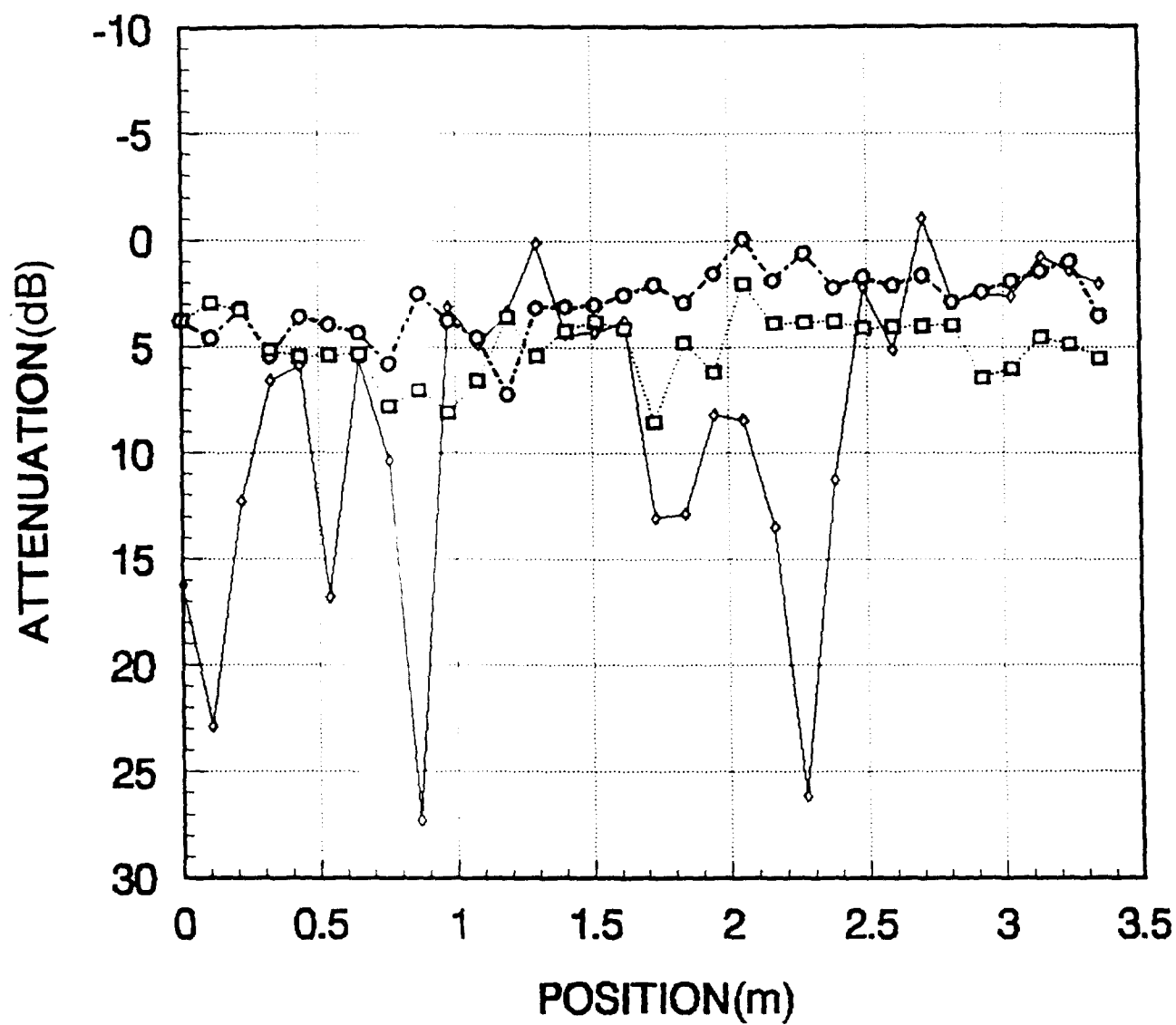
Figure A-18. Penetration loss for Radio Building path RB9B.



**RB10A
ATTENUATION**

◆ 900 MHz
○ 11.4 GHz
□ 28.8 GHz

Figure A-19. Penetration loss for Radio Building path RB10A.



RB10B ATTENUATION

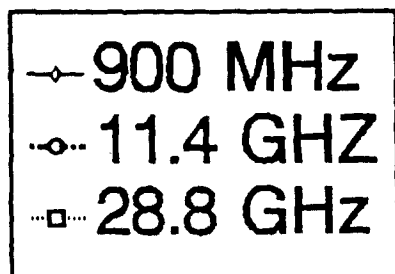
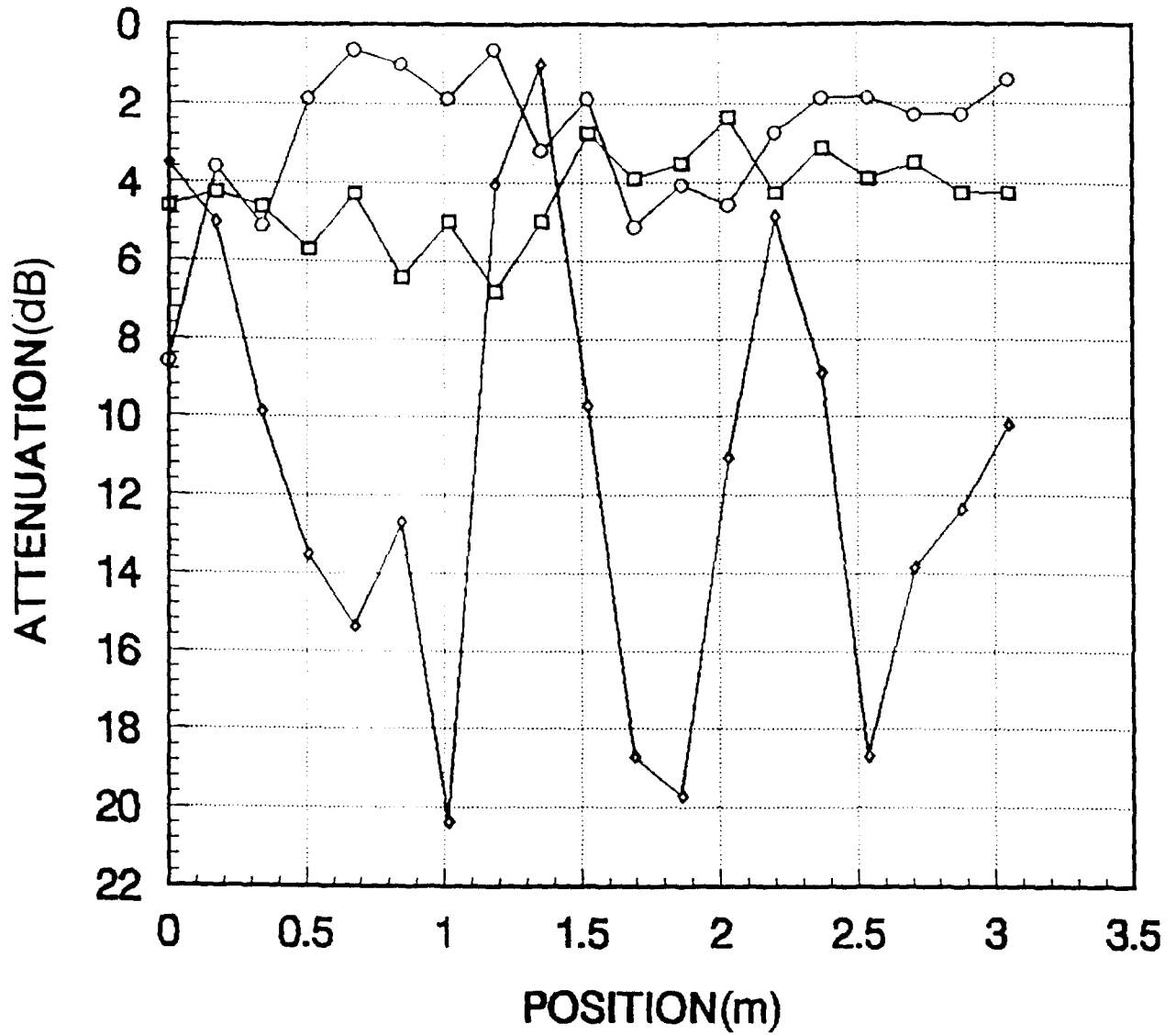


Figure A-20. Penetration loss for Radio Building path RB10B.



**RB11A
ATTENUATION**

◆ 900 MHz
○ 11.4 GHz
□ 28.8 GHz

Figure A-21. Penetration loss for Radio Building path RB11A.